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Jc784 U.S. PRO

**UTILITY PATENT APPLICATION TRANSMITTAL
(Large Entity)**

(Only for new nonprovisional applications under 37 CFR 1.53(b))

Docket No.
96-082-1-US-01

Total Pages in this Submission

55

TO THE ASSISTANT COMMISSIONER FOR PATENTSBox Patent Application
Washington, D.C. 20231

Transmitted herewith for filing under 35 U.S.C. 111(a) and 37 C.F.R. 1.53(b) is a new utility patent application invention entitled:

METHOD FOR PRODUCING A SUBSTANTIALLY CONTINUOUS, NONPOROUS THERMOPLASTIC COATING AND ARTICLES CONSTRUCTED THEREFROMJc530 U.S. PRO
09/584248
05/31/00

and invented by:

ANNEGRET JANSSEN

If a **CONTINUATION APPLICATION**, check appropriate box and supply the requisite information:☒ **Continuation** ☐ **Divisional** ☒ **Continuation-in-part (CIP)** of prior application No.: EP98/01588

Which is a:

☒ **Continuation** ☒ **Divisional** ☐ **Continuation-in-part (CIP)** of prior application No.: DE 19753266.7

Which is a:

☒ **Continuation** ☐ **Divisional** ☐ **Continuation-in-part (CIP)** of prior application No.: _____

Enclosed are:

Application Elements

1. ☒ Filing fee as calculated and transmitted as described below
2. ☒ Specification having 32 pages and including the following:
 - a. ☒ Descriptive Title of the Invention
 - b. ☐ Cross References to Related Applications (if applicable)
 - c. ☐ Statement Regarding Federally-sponsored Research/Development (if applicable)
 - d. ☐ Reference to Microfiche Appendix (if applicable)
 - e. ☒ Background of the Invention
 - f. ☒ Brief Summary of the Invention
 - g. ☒ Brief Description of the Drawings (if drawings filed)
 - h. ☒ Detailed Description
 - i. ☒ Claim(s) as Classified Below
 - j. ☒ Abstract of the Disclosure

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Application Elements (Continued)

3. ☒ Drawing(s) *(when necessary as prescribed by 35 USC 113)*
- a. ☒ Formal Number of Sheets 14
- b. ☐ Informal Number of Sheets _____
4. ☐ Oath or Declaration
- a. ☐ Newly executed *(original or copy)* ☐ Unexecuted
- b. ☐ Copy from a prior application (37 CFR 1.63(d)) *(for continuation/divisional application only)*
- c. ☐ With Power of Attorney ☐ Without Power of Attorney
- d. ☐ DELETION OF INVENTOR(S)
Signed statement attached deleting inventor(s) named in the prior application,
see 37 C.F.R. 1.63(d)(2) and 1.33(b).
5. ☐ Incorporation By Reference *(usable if Box 4b is checked)*
The entire disclosure of the prior application, from which a copy of the oath or declaration is supplied under
Box 4b, is considered as being part of the disclosure of the accompanying application and is hereby
incorporated by reference therein.
6. ☐ Computer Program in Microfiche *(Appendix)*
7. ☐ Nucleotide and/or Amino Acid Sequence Submission *(if applicable, all must be included)*
- a. ☐ Paper Copy
- b. ☐ Computer Readable Copy *(identical to computer copy)*
- c. ☐ Statement Verifying Identical Paper and Computer Readable Copy

Accompanying Application Parts

8. ☐ Assignment Papers *(cover sheet & document(s))*
9. ☐ 37 CFR 3.73(B) Statement *(when there is an assignee)*
10. ☐ English Translation Document *(if applicable)*
11. ☐ Information Disclosure Statement/PTO-1449 ☐ Copies of IDS Citations
12. ☒ Preliminary Amendment
13. ☒ Acknowledgment postcard
14. ☒ Certificate of Mailing
- ☐ First Class ☒ Express Mail *(Specify Label No.):* EK404131055US

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Accompanying Application Parts (Continued)

15. ☐ Certified Copy of Priority Document(s) (if foreign priority is claimed)

16. ☐ Additional Enclosures (please identify below):

Fee Calculation and Transmittal

CLAIMS AS FILED

For	#Filed	#Allowed	#Extra	Rate	Fee
Total Claims	20	- 20 =	0	x \$18.00	\$0.00
Indep. Claims	4	- 3 =	1	x \$78.00	\$78.00
Multiple Dependent Claims (check if applicable) <input type="checkbox"/>					\$0.00
BASIC FEE					\$690.00
OTHER FEE (specify purpose)					\$0.00
TOTAL FILING FEE					\$768.00

- ☐ A check in the amount of _____ to cover the filing fee is enclosed.
- ☒ The Commissioner is hereby authorized to charge and credit Deposit Account No. 06-2241 as described below. A duplicate copy of this sheet is enclosed.
- ☒ Charge the amount of \$768.00 as filing fee.
- ☒ Credit any overpayment.
- ☒ Charge any additional filing fees required under 37 C.F.R. 1.16 and 1.17.
- ☐ Charge the issue fee set in 37 C.F.R. 1.18 at the mailing of the Notice of Allowance, pursuant to 37 C.F.R. 1.311(b).


Signature

Carolyn A. Fischer
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Dated: 5-31-00

CC:

CERTIFICATE OF MAILING BY "EXPRESS MAIL" (37 CFR 1.10)Applicant(s): **A. Janssen**

Docket No.

96-082-1-US-01

Serial No.

Unknown

Filing Date

5/31/00

Examiner

Unknown

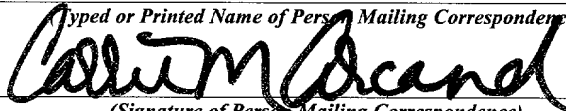
Group Art Unit

Invention:

METHOD FOR PRODUCING A SUBSTANTIALLY CONTINUOUS, NONPOROUS THERMOPLASTIC COATING AND ARTICLES CONSTRUCTED THEREFROMI hereby certify that this **CIP Application***(Identify type of correspondence)*

is being deposited with the United States Postal Service "Express Mail Post Office to Addressee" service under

37 CFR 1.10 in an envelope addressed to: The Assistant Commissioner for Patents, Washington, D.C. 20231 on

May 31, 2000*(Date)***Carrie M. Arcand***(Typed or Printed Name of Person Mailing Correspondence)**(Signature of Person Mailing Correspondence)***EK404131055US***("Express Mail" Mailing Label Number)***Note: Each paper must have its own certificate of mailing.**

IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

Applicant: Janssen

Examiner:

Serial #:

Group Art Unit:

Filed: May 31, 2000

Docket: 96-082-1

Title: **METHOD FOR PRODUCING A SUBSTANTIALLY CONTINUOUS
NONPOROUS THERMPLASTIC COATING AND ARTICLE CONSTRUCTED
THEREFROM**

Honorable Commissioner of Patent
and Trademarks
Washington D.C. 20231

PRELIMINARY AMENDMENT

In the Specification

At p. 1, line 8, insert

“Related Applications

This application is a continuation-in-part of PCT/EP98/01588 filed March 18, 1998, which claims priority to DE 197 53 266.7, filed December 1, 1997.”

At p. 25, line 18, replace “diagram” with --Figure 11--.

At p. 25, line 18, replace “diagram” with --figure--.

At p. 27, line 35, insert;

“In order to demonstrate the improvement in gloss that can be obtained with the present invention, laminations were prepared with the same substrates using both a hot melt adhesive and a waterbase adhesive. The hot melt adhesive composition comprised 4 wt-% A-C 540 Copolymer (ethylene acrylic acid

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copolymer), 56.5 wt-% Escorene UL 15019 CC (ethylene vinyl acetate copolymer), 18.7 wt-% Escorez 5000 (DCPD tackifying resins), 0.4 wt-% Irganox 1010 FF, 0.2 wt-% Irganox 1076 FF, Irganox PS800 FL, 10 wt-% Kristalex F100 (alpha methyl styrene tackifying resin) and 10 wt-% Lotryl 35 BA 320 (ethylene n-butyl acrylate copolymer). The hot melt adhesive had a Ring & Ball Softening Point of 95°C and a Brookfield viscosity of 20,000 mPas at 175°C. The hot melt adhesive was coated onto 12 micron orientated polypropylene film (OPP) with the non-contact coating method, as previously described, at a coat weight of 8 g/m². The adhesive OPP was then contacted and bonded to printed paperstock. The same film and printed paperstock were also laminated with a waterbase adhesive using conventional application techniques. The gloss of the samples was measured with a BYK-Chemie Tri-Gloss Multi-Angle Reflectometer according to ASTM D-523 employing a 20° angle. The gloss values were as follows:

	Example 9 Medium Grey	Example 10 Off-White	Example 11 Light Blue
Paper – no film/ no adhesive	5.3	7.0	5.5
Paper/Film – no adhesive	8.8	12.0	27.2
Waterbase Adhesive	42.9	41.2	48.5
Hot Melt Adhesive	63.6	73.4	64

Gloss is a measure of the capacity of a surface to reflect light in a mirror-like manner. The light is reflected at an equal but opposite angle as the angle of

incidence. Accordingly, in the case of laminations having a transparent film, the gloss value is dependent to some extent on the color of the printed paperstock. Dark colors tend to absorb light, resulting in lower gloss values in comparison to lighter color. In general, however, it is evident from the test results that the adhesive contributes significantly to the overall gloss. Further, the hot melt adhesive is amenable to higher gloss measurements in comparison to the water base adhesive. The improvement in gloss ranges from about 10% to in excess of 75%, depending on the color of the printed paper stock.

Additional laminations of transparent film and printed paper were prepared with other substrates. Examples 12 and 13 employ a 135 g/m² printed carton stock for the production of an automobile poster. The adhesive composition and application technique of the present invention advantageously produces high gloss values for black print. Examples 14 and 15 employ a blue ink that tends to be bleached by conventional water borne acrylic laminating emulsions. Example 16 represents a lamination for use as a magazine cover in which a 120 g/m² printed carton stock was laminated to a 8 micron PET film with 10 g/m² of the adhesive. Example 17 represents a digital print lamination. Digital printing is produced by precipitating ink powder onto paper, similar to a copying machine. The gloss results for each of these examples are as follows:

	Printed Paper	Paper/Film	Paper/Adhesive/Film
Example 12 Light gray	1.4	37.2	59.2
Example 13 Black	5.3	23.4	60.1
Example 14 Light Blue	1.4	9.1	65.5
Example 15 Dark Blue	4.1	63.1	78.9
Example 16 Medium Blue	N/T	N/T	36.6

Example 17 Green	N/T	N/T	49.2
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N/T – not tested

In the Claims

Cancel claims 2-5, 7-9, 11-14, 17-18, 20, and 24-25 without prejudice.
Amend claims 15 and 23 to depend from claim 10 and amend claims 16, 19, 21-22 and 26-28 to depend from claim 1. Add claims 29 to 36 as follows:

~~29.~~ A lamination comprising a transparent film bonded to a substrate with a continuous coating of a hot melt adhesive composition wherein said coating is free of flaws.

30. The lamination of claim 29 wherein said substrate is selected from the group consisting of printed paper, processed photographic paper, and printed cardboard.

31. The lamination of claim 29 wherein the hot melt adhesive is transparent.

32. The lamination of claim 29 wherein the gloss, readability, and color of the substrate is not impaired.

33. The lamination of claim 29 wherein coating has an area weight of less than about 30 g/m².

34. The lamination of claim 29 wherein coating has an area weight of less than about 10 g/m².

35. The lamination of claim 29 wherein the gloss of the lamination ranges from about 10% to in excess of 75% higher than a lamination prepared with the same substrates bonded with a waterbase adhesive composition.

36. The lamination of claim 29 wherein the substrate is digital print.

REMARKS

Upon entry of the amendments to the claims, claims 1, 6, 10, 15-16, 19, 21-23, and 26-36 are pending. Support for claims new 29-33 are supported in the specification at p. 14, line 34 through p. 15, lines 7-9; p. 6, lines 25-31 and the examples at p. 23-27. Claims 35 and 36 are supported by p. 3 of the amendments requested to the specification.

Respectfully submitted,

5-31-00
Date

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5 Method for producing a substantially continuous, nonporous thermoplastic coating and articles constructed therefrom

10 Field of the invention

This invention relates to a non-contact coating method for producing a substantially continuous coating and articles constructed therefrom. The invention further relates to a non-contact slot coating method for producing a variety of coatings and laminations. This invention particularly relates to a method of coating a substrate including film, foil and paper with a molten thermoplastic composition which reduces streaking caused by particles and enables film-to-film, film-to-foil and film-to-paper or board laminations with nonreactive hot melt adhesives.

Background of the invention

25 Conventional slot nozzle coating of molten thermoplastic compositions onto substrates is typically done by keeping the slot nozzle in contact with the substrate such that the nozzle lies on the substrate during the coating. It is unproblematic to coat hot melt adhesives at low coating weights provided that the coating need not be completely closed, i.e. nonporous. In the context of this specification, "continuous" may be used to describe a completely closed, i.e. nonporous film or coating. If, however, a completely closed, i.e. nonporous coating is to be created, this can only be done using customary coating methods if the coating weight of the hot melt is substantially higher.

40 Such high coating weights are expensive. Furthermore, direct coating with a slot nozzle provides substantial

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- 5 mechanical and thermal stresses on the coated substrates, especially since the slot nozzle is heated during coating. Therefore, very sensitive substrates such as plastic films can not always be coated with a hot melt from a slot nozzle in a customary manner without damaging the substrate.
- 10 Further, the high coating weights of this prior art lead to increased stiffness of the coated substrate.

- WO 96/25902, published Aug. 29, 1996, assigned to the H.B. Fuller Co. in St. Paul, MN teaches a method of coating
- 15 wherein certain thermoplastic compositions are thermally made flowable and released from a coating device as a continuous coating without contact between the coating device and substrate being coated.
- 20 The present invention resides in specific adaptations to this novel coating method for use in a variety of other applications involving coatings on nonporous materials and coatings on porous materials. One type of such application is coatings on nonporous materials such as films.
- 25 Thermoplastic compositions often contain unmelted particles either in the form of impurities such as contaminants and char or alternatively in the form of a particulate ingredient such as filler and additives. When these particles are of appreciable size and/or the slot nozzle has
- 30 a relatively small gap, the particles tend to accumulate in the coating device interfering with the deposition of the coating. The particles block the passage of thermoplastic material causing a corresponding striation or streak to form on the substrate being coated. This problem is particularly
- 35 prevalent in the formation of very thin coatings particularly when the optical quality is of importance such as for high quality graphic art applications, especially where films have to be coated. Accordingly, industry would find advantage in a coating method which rectifies these

5 problems.

It is therefore an important object of this invention to provide a new coating method especially suited for coatings on films, foils, paper and other such materials, which makes
10 it possible to avoid streaking and striation problems, especially at very low coating weights.

It is another important object of the invention to provide a coating method which permits laminations and coatings to be
15 carried out „inline“ or „offline“, using thin films, metallized foils, heat-sensitive materials and other sensitive substrates at reduced risk of obtaining faulty or flawed products.

20 It is yet another important object of the invention to make film-to-film and film-to-foil laminations available which do not require the use of reactive adhesives.

Another object of the invention is to provide improved
25 coating methods for coating thermoplastic compositions, especially hot melt adhesives, onto porous substrates such as textiles.

These and other objects and advantages of the invention will
30 become more apparent from the following discussion.

Summary of the invention

35 The present invention is a method of coating a substrate with a thermoplastic composition employing a non-contact coating method and articles constructed therefrom. The method produces a substantially continuous coating. The method is useful for a variety of adhesive and coating

- 5 applications and particularly those which employ conventional slot coating techniques, heat sensitive substrates, require low coating weights, and/or employ thermoplastic compositions comprising particles.
- 10 In one aspect, the present invention is a method of coating wherein a certain thermoplastic composition such as a hot melt adhesive which has been thermally made flowable, is released from a coating device onto a nonporous substrate as a substantially continuous coating without contact between
- 15 said coating device and said substrate, and subsequently disposed upon the surface of the substrate.

In another aspect, the present invention is a method of coating wherein a certain thermoplastic composition such as

20 a hot melt adhesive which has been thermally made flowable, is released from a coating device onto a substrate as a substantially continuous coating without contact between said coating device and said substrate, and subsequently disposed upon the surface of the substrate, wherein the

25 distance between the coating device and the substrate is greater than 20 mm.

In another aspect, the present invention is a method of coating wherein a certain thermoplastic composition such as

30 a hot melt adhesive, which has been thermally made flowable is provided in the form of a substantially continuous nonporous film without contact of the film with a substrate, and said film is then coated onto a substrate by means of either a release-coated roller in direct contact with the

35 adhesive film, said roller nipping said adhesive and said substrate, or with a release coated second substrate being disposed upon the surface of the thermoplastic composition which is not in contact with the first substrate, or by a transfer-coating method, wherein a certain thermoplastic

5 composition such as a hot melt adhesive which has been
thermally made flowable, is released from a coating device
e.g. onto a release coated roller as a substantially
continuous coating, i.e. a nonporous film, without contact
between said coating device and said roller, and
10 subsequently disposed upon the surface of a substrate.

In another aspect, the present invention is a method of
coating wherein a certain thermoplastic composition such as
a hot melt adhesive which has been thermally made flowable,
15 is released from a coating device onto a first substrate as
a substantially continuous coating without contact between
said coating device and first said substrate, and
subsequently disposed upon the surface, wherein said coating
is subsequently reheated and then contacted to a second
20 substrate.

The invention further relates to utilizing this method for
lamination, especially laminating of materials such as
transparent film material, to a substrate, especially a
25 printed paper or cardboard substrate as well as film to film
and film to foil laminations, which avoids the above-
mentioned disadvantages of the prior art and makes it
possible to use nonreactive hot melt adhesives for such
film-to-film and film-to-foil laminations.

30 For heat sensitive substrates, the thermoplastic composition
is preferably coated at temperatures of less than about
160°C, even more preferably less than about 125°C, and most
preferably less than about 110°C to reduce the heat-induced
35 stresses on the substrates being coated. Alternatively, the
distance between the coating device and the substrate to be
coated may be increased such that the molten thermoplastic
composition has sufficiently cooled prior to contacting the
heat sensitive substrate. This is particularly advantageous

The thermoplastic composition preferably exhibits certain rheological characteristics such that the complex viscosity at high shear rates (1,000 rad/sec) is less than about 500 poise and the complex viscosity at low shear rates (1 rad/sec) is less than about 1,000 poise at the coating temperature. Some neat thermoplastic resins are suitable for the method of the present invention provided the uncompounded materials are sufficiently low enough in viscosity. However, compounded hot melt adhesives are preferred due to the ability to independently control the viscoelastic properties, open time, etc. Compounded hot melt are also advantageous to insure adequate adhesion to the carrier substrate or for delayed detackification of the coating after adherence to the substrate.

The resulting coating is preferable for producing laminations to paper or cardboard, especially to printed paper. The coating method is particularly advantageous for manufacturing as it employs fewer production steps than prior art coating methods. Improving productivity as well as reducing the coating weight mass per area results in coatings and corresponding articles that are less expensive

5 than prior art.

The coating methods are however not restricted to applications involving nonporous substrates. The inventive coatings can also be used on porous substrates. Herein,
10 various aspects of the invention can be employed, including a method where the thermoplastic composition is released from a coating device with the distance between the coating device and the substrate greater than 20 mm, and including the method of nipping a hot melt adhesive preformed film to
15 a porous substrate by means of a release coated roller in direct contact with the adhesive film.

Articles as described herein comprise articles which have at least one first layer wherein said first layer is a
20 nonporous substrate and at least one second layer wherein said second layer is a coating or adhesive layer produced from the coating methods described above.

25 **Brief description of the drawings**

Figs. 1-10 depict some of the preferred embodiments of the method of the present invention wherein a substantially continuous thermoplastic coating is formed and adhered to a
30 substrate.

More specifically, Fig. 1A shows the basic structure of a coating and laminating machine useful for operating the invention;
35

Figs. 1B and 1C show the basic structures of similar such machines;

Figs. 2-4 illustrate inventive laminations at different

5 positions of the coating device;

Figs. 5A and B illustrate a lamination and a transfer-coating method according to the invention;

10 Figs. 6-10 illustrate laminations, including adhesive reactivation laminations, in accordance with the invention.

Detailed description of the invention

15 In the method of the present invention, a molten thermoplastic composition, such as a hot melt adhesive, preferably substantially air-free, is initially provided in the form of a substantially continuous, nonporous „film“
20 which is only later contacted with a substrate, a transfer roller or some other kind of support. Generally, the composition is released from a coating or release device in such a way that it exits the device as a substantially continuous film. A typical coating device is a slot nozzle,
25 as it has previously been used for coating in direct contact with substrates. Thus, hot melt coating devices which are already known can be employed in accordance with the method of the present invention in that the slot nozzle is lifted off the substrate and is adjusted to have a suitable
30 distance from the substrate.

As the flowable molten adhesive or thermoplastic composition exits the coating device, it does not contact the substrate, but rather travels for a distance as a continuous film
35 suspended between the coating device and the substrate. The coating device may be initially contacted to the substrate in order to anchor or adhere the thermoplastic composition to the substrate provided that substrate will not be thermally or mechanically damaged by the contact with the

5 coating device. Alternatively, the thermoplastic composition exits through the nozzle as a substantially continuous film and descends until contacting the substrate. The leading edge of the advancing substantially continuous film of thermoplastic composition adheres or anchors to the
10 substrate upon contact with the substrate. In the case of heat sensitive materials, it is advantageous to advance the substrate by means of the drive rolls prior to contacting the thermoplastic composition to the substrate to avoid a build up of molten material which will melt through the
15 substrate.

Machinery suitable for operating the inventive methods is shown schematically in Figures 1A, 1B and 1C. Figures 1A and 1B show an embodiment where a thermoplastic composition
20 is released from a coating device (3) onto a first substrate (1), and a second substrate (4) is then disposed upon the free surface of the coated adhesive, by a nip roll (5). It is to be understood that this arrangement can be modified in other embodiments and especially that the second substrate
25 (4) need not be used in all cases. Then, the nip roll (5) can be employed to nip the thermoplastic composition directly to the first substrate. For such embodiments, the nip roll (5) will be release-coated, e.g. may be a steel roller with a polytetrafluorethylene surface layer.

30

More specifically shown in Fig. 1A and 1B, Substrate 1 (1) travels past a series of idle rollers (2) to ensure the web is in proper alignment prior to approaching the coating device (3). Substrate 2 (4) is optionally adhered to the
35 coating surface by means of a nip roll (5). Substrate 1 is defined as the first substrate that is contacted with the substantially continuous thermoplastic film. Substrate 1 may be any substrate which is generally provided in a roll good such as nonwoven, paper including release-coated paper,

5 and a wide variety of films, foils and other materials. The
embodiment of Fig. 1A, where the nip roll (5) is located
fairly remote from the contact point of adhesive film and
first substrate, is especially suited for the coating of
porous substrates. The embodiment of Fig. 1B is especially
10 suitable when Substrate 1 is nonporous meaning air does not
readily pass through the substrate. In the case of film
lamination, Substrate 1 is typically a film. Substrate 2
may also be provided in a roll good and be the same or a
different material as Substrate 1. However, Substrate 2 may
15 also be a particulate substance such as superabsorbent
polymer, or a release-coated web material that can be pulled
off the adhesive coating.

Fig 1C shows an embodiment where the adhesive film is first
20 nipped onto the first substrate (1) by nipp roll (5), which
is part of a nipping station as later shown by rolls A and B
in Figs. 2-10.

A second substrate 4 is then disposed on the free surface
25 not in contact with the first substrate (1), at a lamination
station formed by folls C and D.

Figs. 2-10 illustrate various preferred embodiments of the
present invention wherein an extruded thermoplastic
30 composition such as a hot melt adhesive is applied to a
first substrate and then laminated to a second substrate.
In each of these illustrations, Substrate 2 is optional in
that the invention in its broadest aspect is simply a single
continuous nonporous film formed from a non-contact coating
35 method and coated onto a single substrate. In the absence
of the second substrate, Figure 5B represents a transfer
coat application since the molten composition is first
applied to a release coated roller which then contacts a
first substrate at the nip.

5 In embodiments where the thermoplastic coating or hot melt
adhesive is contacted to a first substrate in the absence of
a second substrate, as illustrated in Figures 6 and 7, or in
the case when the second substrate is porous, it is
important to have a release coating such as silicon, Teflon,
10 or release paper on the roller(s) in contact with the
adhesive or porous substrate to prevent adherence of the
thermoplastic composition to the roller. The nip roller
presses the air out from between the thermoplastic coating
film and the substrate to insure there is no air entrapment
15 between the first substrate and the thermoplastic
composition. Roller A can be a steel cylinder to encourage
heat transfer whereas roller B, typically the nip roller is
rubber. In some cases it can be more preferred that roller
A is rubber whereas roller B is a steel cylinder with an
20 external release-coating.

Figs. 3-10 demonstrate that the nozzle position may be
varied from perpendicular positions to parallel positions
with respect to the position of the substrate.

25 Figs. 8 and 9 illustrate a second substrate being laminated
to the first substrate at a position farther from the
coating device. In this embodiment, it is preferred that
roller C be heated to reactivate or extend the open time of
30 the hot melt adhesive or thermoplastic coating prior to
being laminated to the second substrate. The temperature of
roller C can vary between about 30-100°C for lamination
between rollers C and D. Alternatively, roller C may be a
chill roll to hasten the speed of set of the thermoplastic
35 coating or hot melt adhesive. This can be useful where the
laminate is produced for intermediate storage. The substrate
laminated in the nip of rollers can be either in web form,
or in the form of sheets. As shown in Fig. 10, where roller
C is a chill roll, the inventive method can be used to

5 produce substrates such as films coated on one side with a
thermoplastic composition, which can e.g. be used for heat
sealing applications. Where this is desired, a further layer
of a release paper can of course be added, as shown in Fig.
9, to protect the heat-sealing material e.g. for
10 intermediate storage.

The coating device is positioned at a distance of at least
0.5 mm, preferably at least 2 mm, from the substrate (or the
release coated roller in the case of transfer coating in the
15 absence of a second substrate - Fig. 5B). The maximum
distance the coating device may be positioned from the
substrate is only limited by practicality, particularly when
the coating device is positioned substantially vertically.
Preferably, the distance is less than about 5 m, preferably
20 less than about 3 m, more preferably less than about 1 m,
even more preferably less than about 500 mm, and most
preferably from about 2 to 20 mm, depending on the
properties of the thermoplastic composition being coating.
It is typically advantageous that the area between the
25 coating device and substrate be shielded during coating from
air-borne contaminants and air currents to prevent
distortion of the coating prior to contacting the substrate.
This is particularly the case when the distance between the
coating device and substrate is greater than about 500 mm.

30

The distance is largely dictated by the viscosity and open
time of the thermoplastic composition being coated. In the
case of producing barrier films in this manner, it is
surmised that the thermoplastic composition cools
35 sufficiently in its suspended state such that it has built
in viscosity and cohesive strength to the extent that any
filaments or fibers present on the substrate surface cannot
penetrate the coating, yet the thermoplastic composition is
molten enough to adequately adhere to the substrate. The

5 greater the distance between the coating device and the nip roller, the more the hot melt adhesive or coating will cool prior to contacting the first substrate. For some adhesive compositions, this cooling will adversely affect the adhesion (or anchorage) to the substrate. Therefore, the
10 substrate may be passed over a heated roller prior to being nipped, or a heated nip roller may be employed if the distance between the nip roller and the coating device causes the coating or adhesive to cool to the extent that it will no longer adequately adhere or anchor to the substrate.

15 The coating may contact the substrate at any angle (compare e.g. Fig. 3 and 4). However, it has been shown to be especially advantageous for some applications such as for barrier films, that the coating later contacts the substrate
20 in a substantially horizontal direction as in Fig. 1A, 1B, 2, 6 and 8. To accomplish this, a roller can be provided in the path of movement of the substrate to give the substrate a substantially vertical, upward direction, as the substrate passes the coating device. Additionally, the coating
25 device, such as a slot nozzle, can be provided substantially horizontally beside the roller so that the coating travels from the side towards the surface of the substrate.

The diameter of the coating roller is preferably about 15 mm
30 to about 50 mm in diameter with the nozzle slightly above the center of the coating roll such that the angle at which the thermoplastic coating contacts the substrate is less than about 60° as the substrate is moving away from the nozzle. The coating head is adjusted by one of ordinary
35 skill in the art to optimize for even flow and distribution of the thermoplastic coating over the entire width of the application.

Thereafter, the sufficiently cooled coating contacts the

5 substrate surface and adheres to the surface without deeply
penetrating into the substrate. If the thermoplastic
coating is of such a composition that it substantially
detackifies after sufficient cooling, the laminate of the
coated substrate, thus formed, can be rolled up and stored.
10 Alternatively this can be achieved by placing a release
coated second substrate, such as a silicone-coated paper, on
the surface of the adhesive coating. The laminate can then
be used at some later time. The laminate can be bonded by
any suitable bonding technique including ultrasonic bonding,
15 heat sealing, or more commonly adhesive bonding.

Preferably, the coating is done "inline" immediately before
any further processing. An example of an in-line process
for which the invention is particularly well suited may be
20 found in DE 195 46 272 C1 to Billhöfer Maschinenfabrik GmbH,
incorporated herein by reference. The surface of the
coating layer which is pointing away from the substrate may
be sufficiently tacky such that it can be used as a
construction adhesive or for lamination to other substrates
25 and therefore can also serve to bond the coated substrate to
another substrate layer. Other substrates that may be
simultaneously bonded or laminated in this manner include
absorbent, superabsorbent polymer, elastomeric strands or
webs, tissue, films, foils, paper, cardboard, metal, as well
30 as various permeable coverstock materials such as nonwoven
or perforated films. These materials may be in the form of
roll-goods, sheets, or particles.

In a preferred embodiment, the substrate to be laminated is
35 paper or cardboard, especially printed paper, processed
photographic paper or printed cardboard, as used in the
production of e.g. book covers, picture postcards,
calendars, posters, high quality packaging materials, gift-
wraps and so forth. The laminating material can be

5 synthetic film material, paper, textile material or any other flexible laminating material suitable for lamination. Preferably, the laminating material is, however, a synthetic film material, especially a clear and transparent film material as is customarily used for such laminations.

10

Typically such film materials comprise plane or embossed films, which are at least substantially made from oriented polypropylene, polyethylene, polyesters such as Mylar®, polyacetate, nylon, celluloseacetate, and so forth having a

15

thickness of about 5 microns to about 50 microns. These films are commonly laminated or sealed to printed paper or boardstock. Composite materials are commonly produced including film to film and film to foil and metallized substrates are commonly used for laminates. These types of

20 laminates are commonly found in such industries as graphic arts and packaging. Using the method of the invention, such laminates can be produced using nonreactive hot melt adhesives instead of the commonly used reactive adhesives.

25

Generally, the exit temperature of the thermoplastic composition will be less than about 240°C, and thus much lower than typical polymer extrusion temperatures, which are of the order of 300°C. Although the temperature of the thermoplastic composition as it exits the coating device may

30

range from about 80°C and about 180°C or more, the non-contact coating system of the present invention allows coating to be accomplished at extremely low temperatures. For this embodiment it is preferred that the thermoplastic composition be coated at a temperature less than 160°C, more

35 preferably less than about 140°C, even more preferable less than about 120°C and even more preferable less than about 110°C. As mentioned previously, heat sensitive materials can also be coated in this manner by employing higher coating temperatures in combination with increasing the

5 distance between the coating device and the substrate to be
coated to allow for sufficient cooling. Materials which are
normally too sensitive mechanically and/or thermally (e.g.
very low gauge films) for customary coating methods can
therefore be coated using the method of the present
10 invention. Such sensitive materials include low gauge
polyethylene materials, low basis weight nonwovens and the
like.

15 A substantial advantage of the present invention is that a
substantially continuous coating layers can be made from hot
melts at very low coating weights. Even with customary
commercially available hot melts, continuous layers can be
produced at coating weights ranging from about 0.5 g/m² to
as much as 50-60 g/m², preferably at coating weights of not
20 more than about 30 g/m², more preferably at coating weights
of not more than 20 g/m², even more preferably between 10
g/m² and 20 g/m² and most preferably less than 10 g/m².
However, coating weights higher than 60 g/m² may be useful
for other applications wherein reducing the mechanical and
25 heat-induced stresses is of primary importance.

The very thin coatings which can be produced according to
the invention not only contribute to the economical
advantages of the inventive method, but also makes it
30 possible to achieve a very much reduced stiffness of the
material, which thus comes much closer, in its properties,
to uncoated substrates.

35 The thermoplastic composition

As previously mentioned various thermoplastic materials may
be used in the present invention such as various
thermoplastic polymers may be used including polyethylene,

5 polypropylene, copolymers of olefins, especially ethylene,
and (meth-) acrylic acid; copolymers of olefins, especially
ethylene, and (meth-) acrylic acid derivatives, especially
(meth-) acrylic acid esters; copolymers of olefins,
especially ethylene, and vinylic compounds, especially vinyl
10 carboxylates such as vinyl acetate; thermoplastic rubbers
(or synthetic rubbers) such as styrene-isoprene-styrene,
styrene-butadiene-styrene, styrene-ethylene/butylene-styrene
and styrene-ethylene/propylene-styrene block copolymers
available in commerce under the tradenames of Kraton®,
15 Solprene®, and Stereon®; metallocene-catalyzed polymers,
especially based on ethylene and/or propylene; polyolefins
such as ethylene, polypropylene and amorphous polyolefins
(atactic poly-alpha-olefins) such as Vestoplast® 703
(Hüls); polyesters; polyamides; ionomers and corresponding
20 copolymers; and mixtures thereof. Such thermoplastic
materials may be employed in the coating method of the
present invention uncompounded provided the thermoplastic
material is sufficiently low enough in viscosity. However,
hot melt adhesives are preferred due to the ability to
25 independently tailor the viscoelastic properties, open time,
tack, and various other properties. Hot melt adhesives
commonly have melt flow indices required for such processing
already at very low temperatures. Typical hot melts are
fluid enough for such processing at temperatures ranging
30 from about 60°C to about 175°C. Additionally, various known
hot melt moisture cure compositions are contemplated for use
in the present invention.

With suitable hot melts, such as those described in DE-A-41
35 21 716, it is also possible to make materials which are
impermeable to liquid water, yet water vapor permeable
rendering the coating "breathable".

5 In addition to commonly known hot melt adhesives,
thermoplastic compositions comprising a water soluble,
saline (body fluid) insoluble polymer such as Eastman AQ
copolyesters, commercially available from Eastman, are also
particularly useful for creating barrier films that are
10 impervious to body fluid, yet readily water soluble. This
feature is of particular interest for creating flushable and
compostable disposable hygienic products. Furthermore,
there may be applications wherein water permeability is
desired. Accordingly, this coating method may also be
15 suitable for coating water soluble and/or biodegradable
thermoplastic materials.

In the case of the lamination adhesives for transparent
substrates, thermoplastic polymers comprising substantially
20 or consisting entirely of one or more
ethylene/methylacrylate copolymers (EMA's) and/or
ethylene/n-butyl acrylate copolymers (EnBA's) is preferred.
EnBA copolymers are presently the most preferred such
polymers.

25 More preferably, the thermoplastic composition exhibits
certain rheological characteristics such that a
substantially continuous coating can be produced at coating
weights of less than about 50-60 g/m² and preferably less
30 than about 30 g/m². In general, the rheological properties
preferably fall within a rheological window wherein the
complex viscosity at the coating temperature at high shear
rates (1,000 rad/sec) is less than about 500 poise and the
complex viscosity at low shear rates (< 1 rad/sec) is less
35 than about 1,000 poise. In other words, preferable
thermoplastic compositions exhibit Newtonian regions at low
shear rates and shear thinning at higher shear rates.
Thermoplastic compositions having wide windows of
application are those in which the composition exhibits the

5 appropriate rheological properties at a variety of
application settings, particularly low application
temperatures. Narrow application windows are those in which
the rheological parameters are only met under very specific
conditions.

10

The applicants surmise the complex viscosity and high shear
relates to the processing conditions at the slot die exit.
A composition with too high of a complex viscosity at 1,000
radians/sec would require excessive pump pressure to exit
15 the coating device. A die with a shim gap larger than 3 mm
could be used to process these materials but a higher
coating weight may result.

The complex viscosity and low shear relates to the settling
20 of the coating on the substrate during the time it is
suspended above the substrate. If the low shear value is
too high, the coating may not adhere adequately to the
substrate and/or the thermoplastic composition builds up at
the nozzle causing a streaked, discontinuous coating. If
25 the low shear viscosity is too low, the coating may seep
into the substrate, causing poor barrier properties.

Extensional viscosity, which was not measured can also
strongly influence the melt strength. Higher levels of
30 branching or the addition of a small concentration of a high
molecular weight material can strongly influence the melt
strength. More preferred, are compositions that meet the
target rheological parameters at low application
temperatures, less than about 177°C, preferably less than
35 about 160°C, more preferably less than about 140°C, even
more preferably less than about 125°C, most preferably less
than about 110°C.

5 Accordingly, many known hot melt adhesive compositions are well suited for use in the coating method of this invention. Hot melt adhesives typically comprise at least one thermoplastic polymer, at least one plasticizer and at least one tackifying resin. Preferably, such suitable hot melts
10 comprise up to 50% by weight of thermoplastic polymer, up to 40% by weight of a plasticizer and up to 70% by weight of tackifying resin. In the case of hot melt adhesives which are not pressure sensitive, wax is generally employed in concentrations up to about 30% by weight of the adhesive.

15 Generally, the invention's hot melts will additionally contain one or more tackifying resins, plasticizers or oils and waxes plus customary additives and adjuncts such as stabilizers, antioxidants, pigments, UV stabilizers or
20 absorbers, fillers etc. Plasticizers and tackifying resins used in hot melt adhesives are known.

Oils such as naphthenic oils are preferred plasticizers. As for tackifying resins, those resins already known for such
25 purposes are generally suitable, especially aliphatic, cycloaliphatic and/or aromatic hydrocarbon resins, ester resins and other such compatible resins. It is presently preferred to use either aliphatic or aromatic modified hydrocarbons resin. The preferred aliphatic resins are
30 hydrogenated aliphatic hydrocarbon resin, for example, the Escorez® 5000 series available from the Exxon Chemical Co. in Houston, TX and the Arkon® P and M series available from Arakawa Chemical Co. and the Regalite® series available from Hercules Inc. in Wilmington, DE. Rosins and rosin
35 ester resins are also useful in the present invention. One such hydrogenated rosin acid tackifying resin is Foral® AX available from Hercules. Modified hydrocarbon resins such as modified terpenes including styrenated terpenes such as

5 the Zonatac® series available from Arizona Chemical Co. in
Panama City, FL and the Kristalex® series of alpha-methyl
styrene resins available from Hercules, Inc. and the
Uratack® series available from Arizona Chemical are also
useful in the present invention. The components are mixed
10 and processed in a known manner to prepare the hot melts
which can be used according to this invention.

Waxes are also useful in the present invention. These
include synthetic high melting point waxes such as Fischer
15 Tropisch waxes available from Sasol (South Africa) under the
tradename of Paraflint®, or from Shell Malaysia under the
tradename Petrolite, and high density low molecular weight
polyethylene waxes available from Marcus Chemical Co. under
the tradename of Marcus®. AC 8 is another useful
20 polyethylene wax available from Allied Chemical.
Microcrystalline waxes and paraffin waxes are also useful to
the present invention.

Laminating adhesives will preferably comprise up to 100% of
25 at least one thermoplastic polymer described above; 0-50% of
an aliphatic hydrocarbon resin; 0-20% of an aromatic
hydrocarbon resin; 0-40% rosin and 0-20% wax, said
components and their amounts being chosen so that the
adhesive is in-line coatable onto a laminating material
30 and/or a laminating substrate, for subsequent in-line
lamination of said laminating material to said substrate.

More preferably, in the case of film laminating, the
adhesive will comprise the following components: up to 100%
35 of at least one EMA and/or EnBA copolymer; 0-50%
hydrogenated aliphatic hydrocarbon resin; 0-20% alpha-methyl
styrene resin; 0-40% hydrogenated rosin and 0-20%
polyethylene wax.

- 5 The hot melt adhesive usable for practicing the invention's method can, in the simplest case, consist substantially or even completely of one or more grades of EMA or EnBA copolymers. EMA and EnBA copolymers are available from Elf Atochem under the Lotryl® tradename, from Quantum Chemical
- 10 Co. and From Exxon Chemical Co. under the Optema® tradename. A variety of different grades of EMA and EnBA copolymers are available. They mainly differ in ester content, melt flow index (MFI) and melting point.
- 15 In presently preferred special embodiments, the hot melt adhesive essentially consists of 35-60% EnBA or EMA; 30-50% hydrogenated aliphatic hydrocarbon resin or about 10% alpha-methyl styrene resin; 0-30% hydrogenated rosin and 0-10% polyethylene wax, plus small amounts of stabilizer. In some
- 20 preferred embodiments, the thermoplastic polymer of the hot melt adhesive is a single grade of EnBA copolymer, usually at the low end of the MFI range (i.e. MFI less than 10 g/10 min.) In other preferred embodiments, the thermoplastic polymer comprises more than one grade of EnBA, and in these
- 25 cases, two or three different grades wherein at least two of the grades preferably have MFI's which differ by at least a factor of 4 and up to a factor of 10 (i.e. one grade has an MFI more than 4 times that of the other grade.
- 30 The inventive hot melts can be used at application temperatures (or processing temperatures) which are low enough to prevent distortion of heat sensitive plastic film, and at the same time show excellent flow properties at such low temperature. It is, for example, possible to coat and
- 35 laminate the inventive hot melt on the laminating materials. Non-contact coating is especially advantageous for heat sensitive films. Excellent film forming performance is achieved, and the laminated products exhibits high glossiness.

5

The laminating adhesives of the invention produce high transparency of the hot melt coating, so that high gloss is achieved, while readability and color rendition of, for example, printing on the substrate is not impaired.

10

The inventive hot melts show excellent (high) hot-tack and open time characteristics for the method of the present invention as well as setting properties. They meet the requirements of machine condition, in-line embossing and cutting, for example, in the graphic arts industry.

15

Laminates made according to the invention exhibit high heat resistance and high UV resistance, and correspondingly little delamination or yellowing. Also after heat forming and embossing, no delamination is observed when the hot melt formulations of the invention are used.

20

The following non-limiting examples further assist in illustrating the present invention.

25

Examples

Hot melt adhesives were produced from different

30

thermoplastic polymers, tackifiers and plastizisers as shown in Table 1 below:

Examples 1-8

TABLE I

Ingredients	Ex 1	Ex 2	Ex 3	Ex 4	Ex 5	Ex 6	Ex 7	Ex 8
Lotryl® 17 BA 07 EnBA copolymer	23	40	35	10	23	-	-	-
Lotryl® 35 BA 40 EnBA copolymer	15	-	-	20	15	20	15	15
Lotryl® 35 BA 320 EnBA copolymer	17	-	-	30	17	10	16	15
Escorene® UL 150-19 EVA copolymer	-	-	-	-	-	20	24	23
AC-8 polyethylene wax	5	10	-	-	5	-	5	-
Paraflint® C 80 polyethylene wax	-	-	-	-	-	10	-	-
MOBIL Wax 145 paraffin wax	-	-	-	-	-	-	-	5
Escorez® 5300 hydrocarbon resin	28	38	38	38	-	23	28	30
Foral® AX rosin acid resin	10	10	25	-	28	15	10	10
Kristalex® F 85 alpha-methyl styrene resin	-	-	-	-	10	-	-	-

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5 Hot melt adhesives corresponding to the compositions
depicted in Examples 1 and 7 were coated onto substrates,
using a modified PAK 600 laminating machine by Kroenert,
Hamburg, Germany. The structure of this machine is
basically similar to that shown in Fig. 1B. With this type
10 of machine, it is possible to nip the adhesive film directly
onto the first substrate (1) by means of nip roller (5) or
nip a second substrate (4) onto the first substrate and
adhesive, again by means of nip roller (5). In the tests,
both methods were tried. The dispensing temperature of the
15 hot melt was 140°C for the composition of Example 1, and
110°C for the composition of Example 7. These compositions
show favourable low viscosities, as is notable from the
attached diagram. This diagram illustrates the viscosities
of Examples 1 and 7.

20 Coatings were made on polyester film (Polyester RN 36,
produced by Pütz Folien, Taunusstein-Wehen, Germany) and
high density polyethylene films (HDPE KC 3664.00, obtained
from Mildenberger + Willing, Gronau, Germany).

25 As a second substrate (where used), these films were also
used. In other experiments, silicone paper was used instead.
Tests were also made with printing paper sheets as the
second substrate.

30 Coating weights were 5 to 6 g/m² at machine speeds of
approximately 70 m/minute.

The adhesive film was released from the coating slot nozzle,
35 at various distances from the first substrate (1) to be
coated with the adhesive, in a variety of tests. In another
set of experiments, With a vertical configuration (similar
to Figs. 3-5, 7, 9 and 10) it was found that the distance of
the slot nozzle from the substrate could be varied between a

5 few millimeters and up to 500 mm and more, without materially affecting the quality of the coating.

Wherein these experiments, the adhesive film released from the coating slot nozzle was directly coated onto the first
10 substrate by means of nip roller (5) provided with a release coating, it was found that the adhesive did not adhere to the nip roller. The nip pressure was not measured, but the nip roller was pressed against the substrate at a laminating pressure of 7 to 8 bar.

15

It was found that the adhesive coated onto the first substrate left the nip station with no air enclosed between the adhesive and the first substrate.

20

In other tests, a second substrate was laminated onto the adhesive layer by a second set of rollers, located in the flow path of the substrate upstream of the nip roller (5). Also these laminations, using the same films, or release-coated paper, as above discussed, were examined for

25

streaking, enclosed air, or other lamination defects.

The laminations thus made were all free of flaws. No streaking, enclosed air or any other defects were observed.

30 In a similar fashion, laminations were made using the same type of films, but the other adhesives depicted in Examples 2 to 6 of Table 1. The results were as good as those obtained with the adhesive compositions of Examples 1 and 7.

35

C L A I M S

5
10 1. A method of coating, wherein a hot melt adhesive, which has been thermally made flowable, is released from a coating device onto a substantially nonporous substrate as a substantially continuous coating without contact between said coating device and said substrate, and subsequently disposed upon the surface of said substrate.

15 2. A method of coating, wherein a hot melt adhesive, which has been thermally made flowable, is released from a coating device onto a substrate as a substantially continuous coating without contact between said coating
20 device and said substrate, and subsequently disposed upon the surface of said substrate, wherein the distance between the coating device and the substrate is greater than 20 mm.

25 3. A method of coating, wherein a hot melt adhesive, which has been thermally made flowable, is provided in the form of a substantially continuous nonporous film without contact of the film with a substrate or a roller, and said film is then coated onto a substrate by means of a release-coated roller in direct contact with the adhesive film,
30 said roller nipping said adhesive and said substrate.

4. A method of coating, wherein a hot melt adhesive, which has been thermally made flowable, is released from a coating device onto a release coated roller as a
35 substantially continuous coating without contact between said coating device and said roller, and subsequently disposed upon the surface of a substrate.

5. A method of coating, wherein a hot melt adhesive,

5 which has been thermally made flowable, is provided in the
form of a substantially continuous nonporous film without
contact of the film with a substrate, and said film is then
coated onto a first substrate, with a release-coated
substrate disposed upon that surface of the hot melt
10 adhesive which is not in contact with the first substrate.

15 6. A method of coating, wherein a hot melt adhesive,
which has been thermally made flowable, is provided in the
form of a substantially continuous nonporous film without
contact of the film with a substrate, and said film is then
disposed upon a release-coated substrate and is then
transfer-coated onto a second substrate.

20 7. A method of coating, wherein a hot melt adhesive,
which has been thermally made flowable, is released from a
coating device onto a first substrate as a substantially
continuous coating without contact between said coating
device and said first substrate, and subsequently disposed
upon the surface of said first substrate, wherein said
25 coating is reheated and then contacted to a second
substrate.

30 8. A method of coating, wherein a thermoplastic
material which has been thermally made flowable, is
provided in the form of a substantially continuous
nonporous film without contact of the film with a substrate
and said film is then coated onto a substantially nonporous
substrate.

35 9. A method of coating, wherein a thermoplastic
material, which has been thermally made flowable, is
released from a coating device at less than about 240°C in
the form of a substantially continuous nonporous film,
without contact of the film with a substrate, and said film

5 is then coated onto a substrate.

10 10. A method of coating, wherein a thermoplastic material, which has been thermally made flowable, is provided in the form of a substantially continuous nonporous film without contact of the film with a substrate and said film is then coated onto a substrate, said coating having a complex viscosity of less than about 500 poise at about 1000 radians/sec at the coating temperature.

15 11. A method of coating, wherein a thermoplastic coating having a complex viscosity of less than about 500 poise at about 1000 radians/sec at the coating temperature has been thermally made flowable is released from a coating device onto a nonporous substrate as a substantially continuous coating without contact between said coating device and said substrate, and subsequently disposed upon the surface of said substrate.

20 12. A method of coating, wherein a thermoplastic coating having a complex viscosity of less than about 500 poise at about 1000 radians/sec at the coating temperature, which has been thermally made flowable, is released from a coating device onto a substrate as a substantially continuous coating without contact between said coating device and said substrate, and subsequently disposed upon the surface of said substrate, wherein the distance between the coating device and the substrate is greater than 20 mm.

25 13. A method of coating, wherein a thermoplastic coating having a complex viscosity of less than about 500 poise at about 1000 radians/sec at the coating temperature, which has been thermally made flowable, is released from a coating device onto a first substrate as a substantially continuous coating without contact between said coating

5 device and said first substrate, and subsequently disposed upon the surface of said first substrate, wherein said coating is reheated and then contacted to a second substrate.

10 14. A method of coating, wherein a thermoplastic coating having a complex viscosity of less than about 500 poise at about 1000 radians/sec at the coating temperature, which has been thermally made flowable, is released from a coating device onto a release coated roller as a
15 substantially continuous coating without contact between said coating device and said roller and subsequently disposed upon the surface of a substrate.

20 15. The method of claims 8 to 14, wherein said thermoplastic coating has a complex viscosity of less than 1000 poise at about 1 radians/sec at the coating temperature.

25 16. The method of claims 1 to 15, wherein said substrate is selected from the group consisting of film, foil, paper and combinations thereof.

30 17. The method of claim 16, wherein said first and said second substrates are selected from films, foils, paper, coated paper, co-extruded films and other laminating materials, and said adhesive is a nonreactive adhesive, or a reactive hot melt adhesive.

35 18. The method of claims 15 or 16, wherein said coated substrate comprises a heat sealing material.

19. The method of claims 1 to 18, wherein said coating device is a slot nozzle.

5 20. The method of claims 1 to 19, wherein said coating has an area weight of less than about 60 g/m².

21. The method of claims 1 to 20, wherein the coating has an area weight of less than about 30 g/m².

10 22. The method of claims 1 to 21, wherein the coating has an area weight of less than about 10 g/m².

15 23. The method of claims 8 to 14, wherein the thermoplastic composition is released from the coating device at a temperature of less than about 160°C.

20 24. The method of claims 8 to 14, wherein the thermoplastic composition is released from the coating device at a temperature of less than about 110°C.

25 25. The method of claims 1 to 24, wherein a first substrate is bonded to at least one second substrate "inline" or "offline".

26. The method of claims 1 to 25, wherein the distance between the coating device and the substrate ranges from about 0.5 mm to 500 mm.

30 27. A book cover made by any one of the methods of claim 1 to 26.

28. A lamination made by any one of the methods of claims 1

35 to 26.

A B S T R A C T

This invention relates to a non-contact coating method for
10 producing a substantially continuous coating and articles
constructed therefrom. This invention further relates to a
non-contact slot coating method for producing a variety of
coatings and laminations. This invention particularly
15 relates to a method of coating a non-porous substrate
including film, foil and paper with a molten thermoplastic
composition which reduces streaking caused by particles
such as impurities, fillers and superabsorbent polymers.
This invention further relates to thermoplastic
20 compositions useful in the present non-contact coating
method.

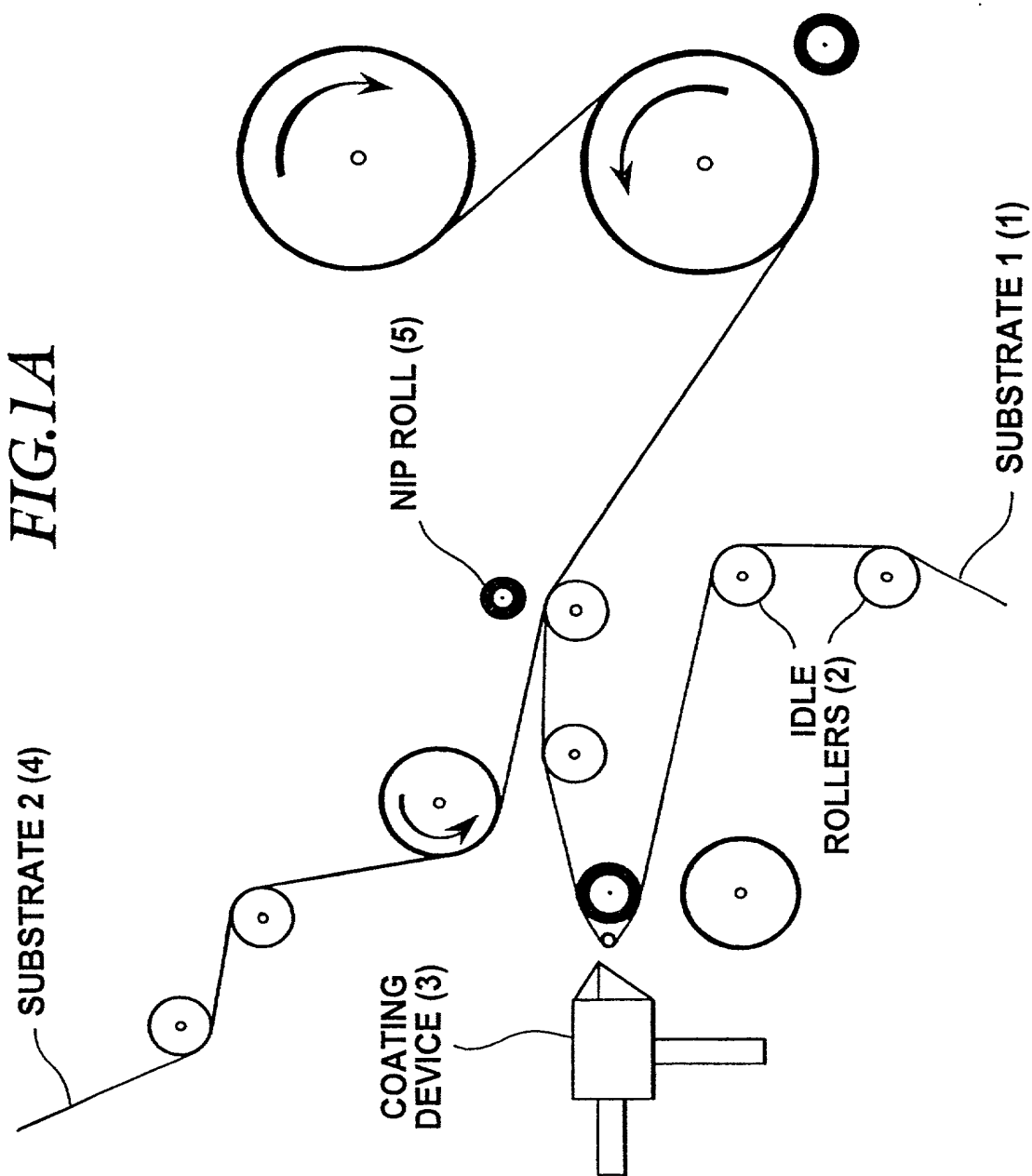


FIG. 1A

FIG. 1B

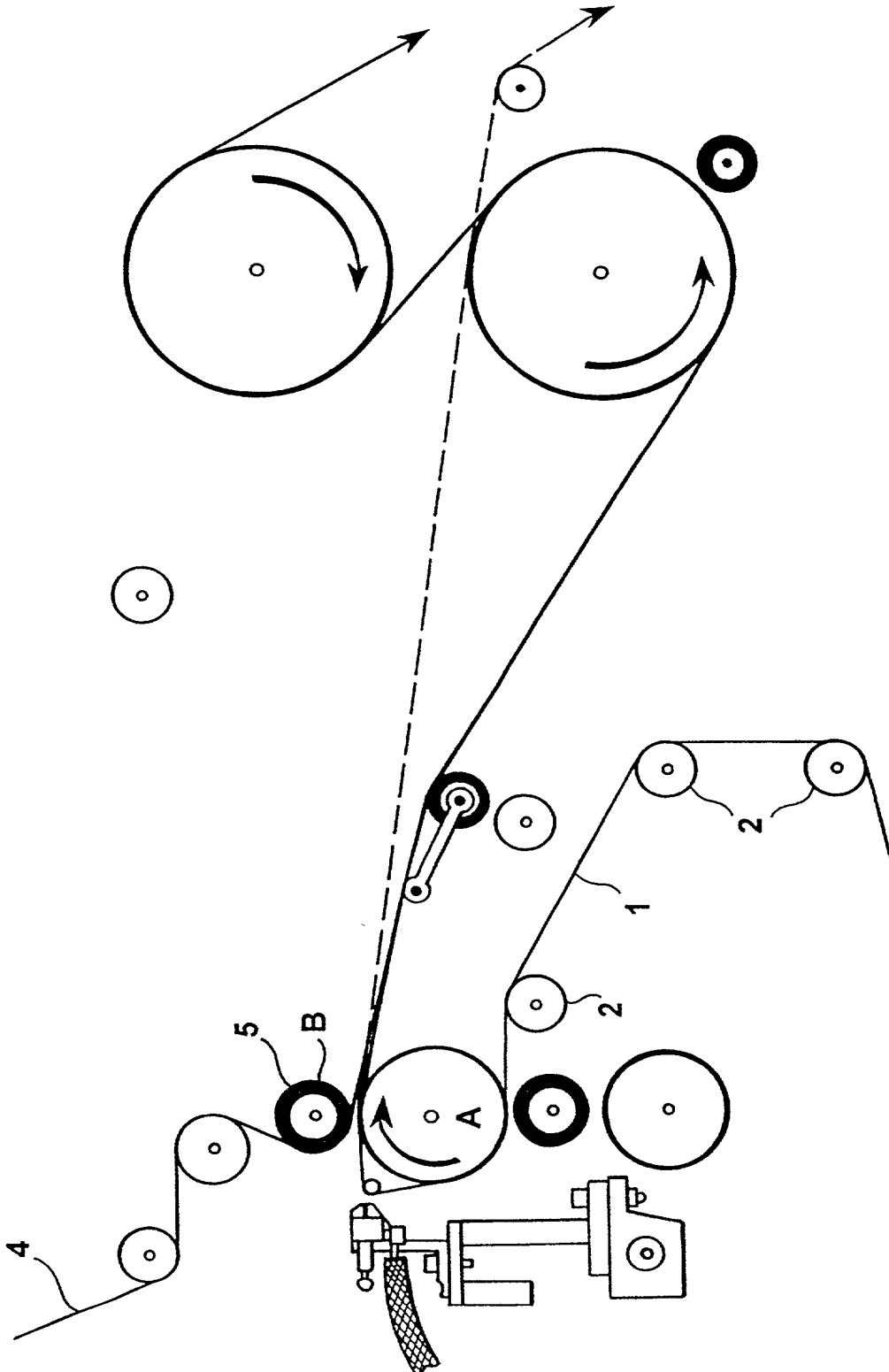


FIG. 1C

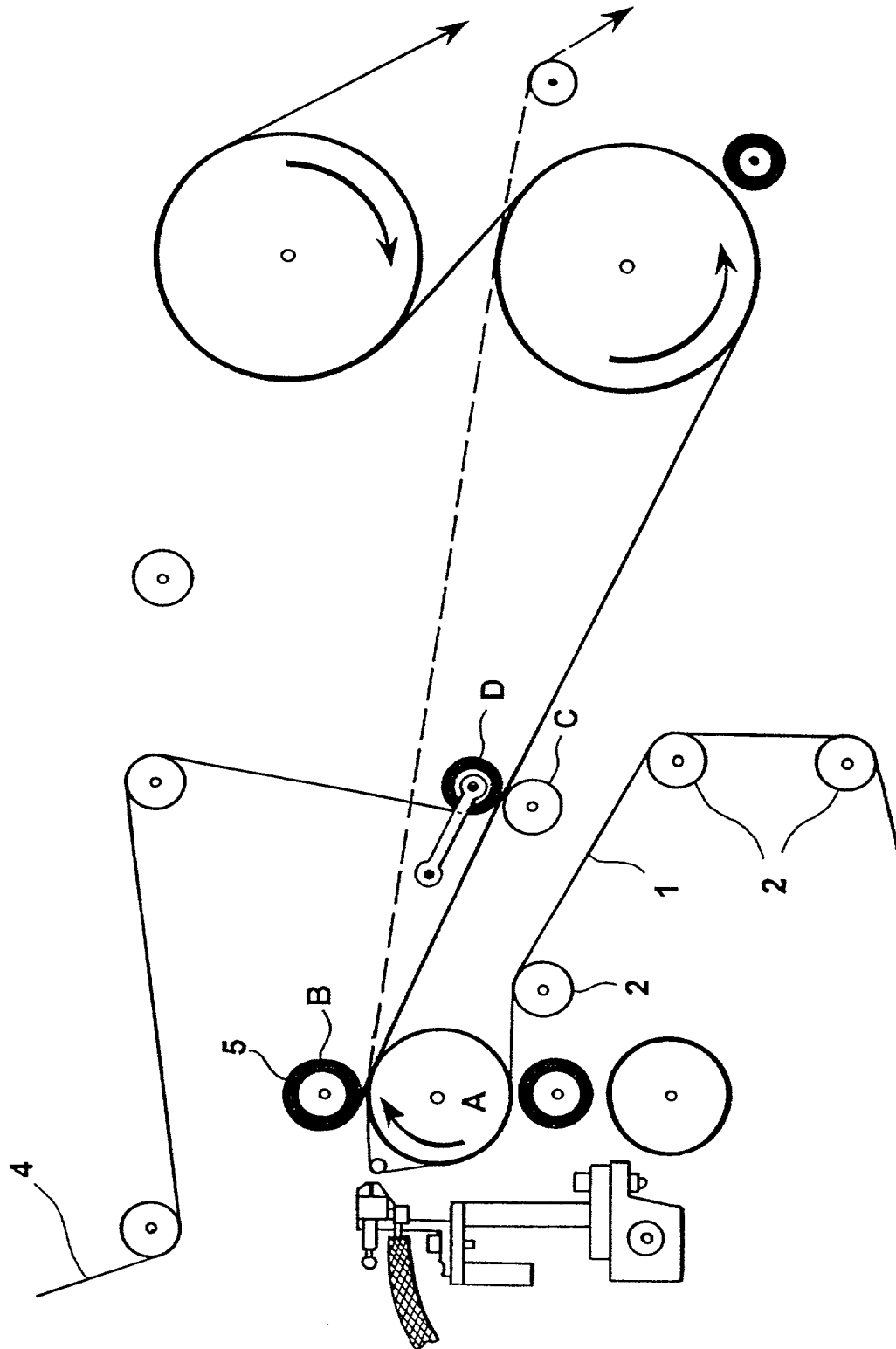


FIG.2

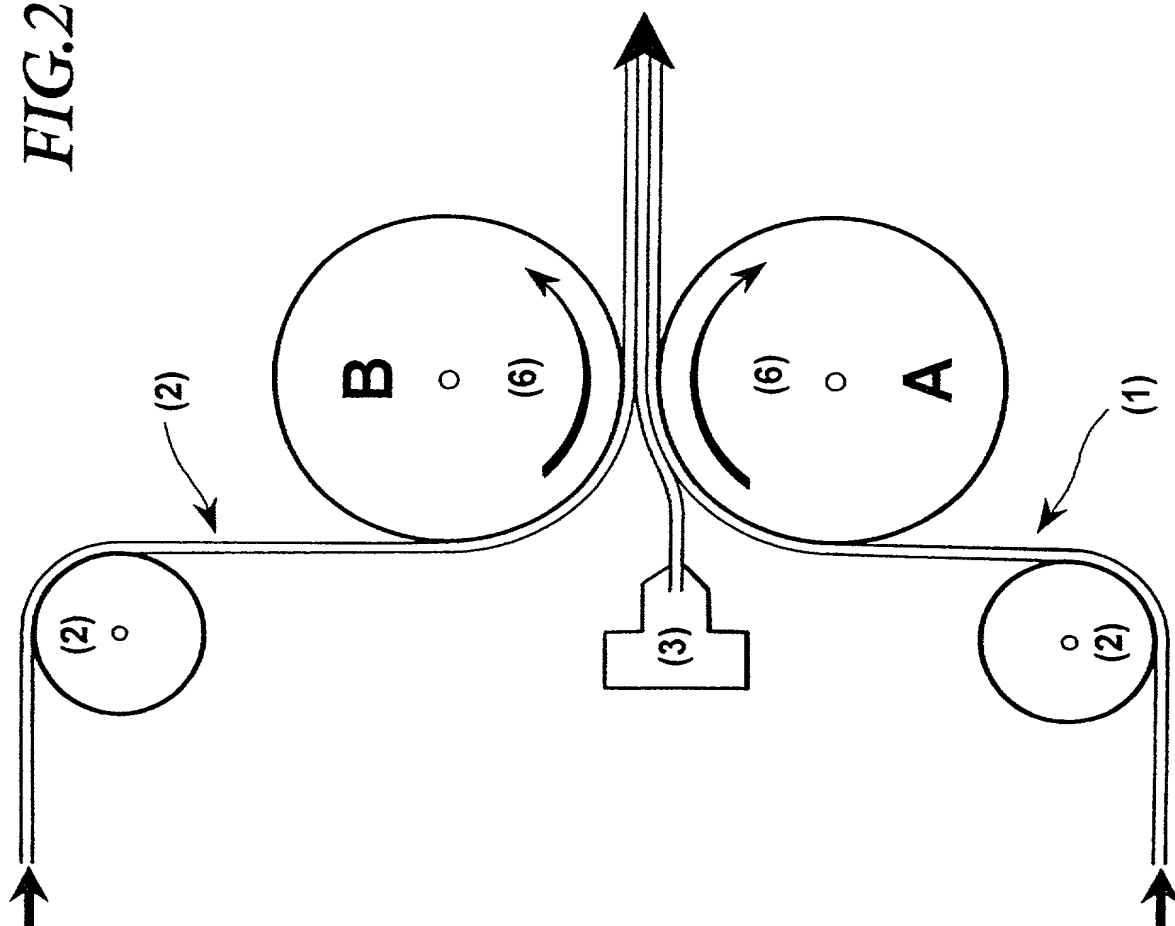


FIG.3

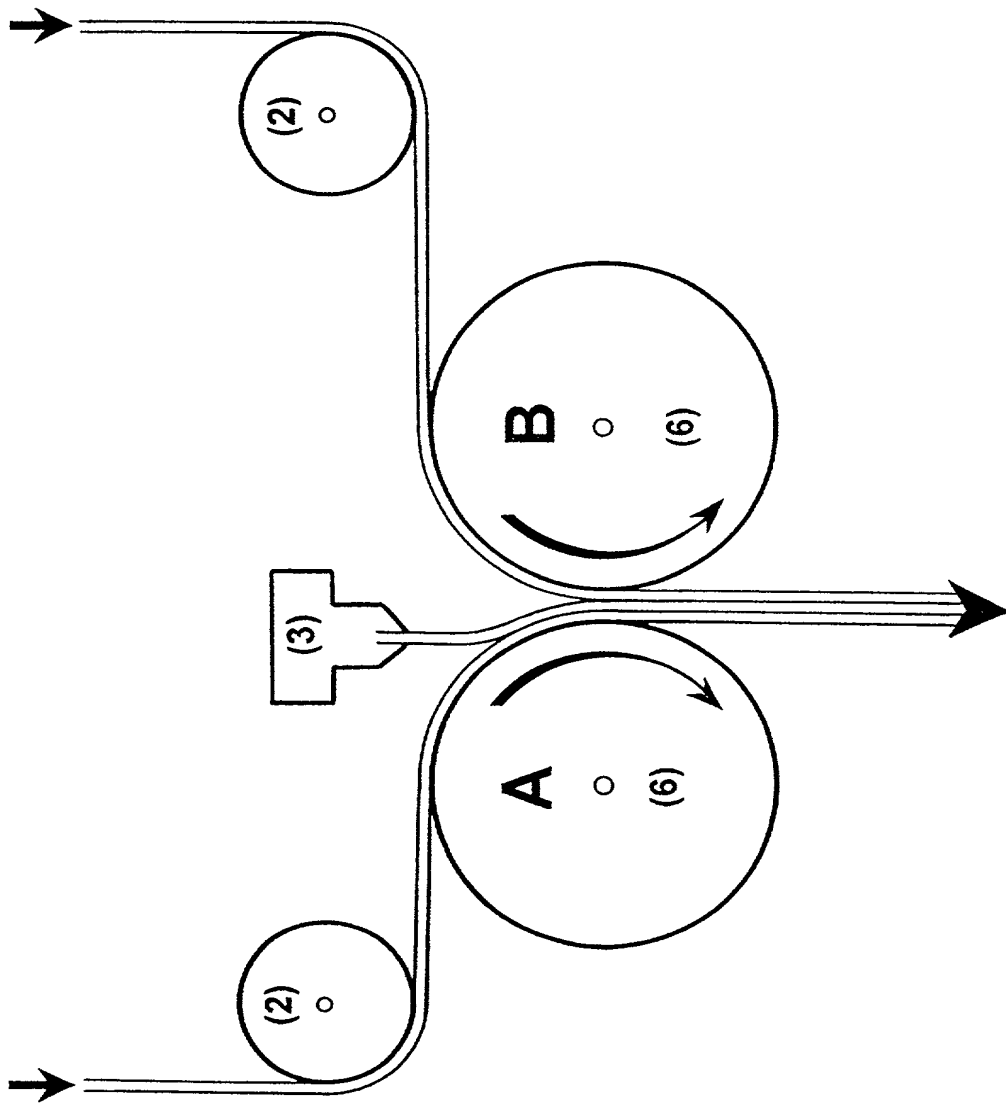


FIG.4

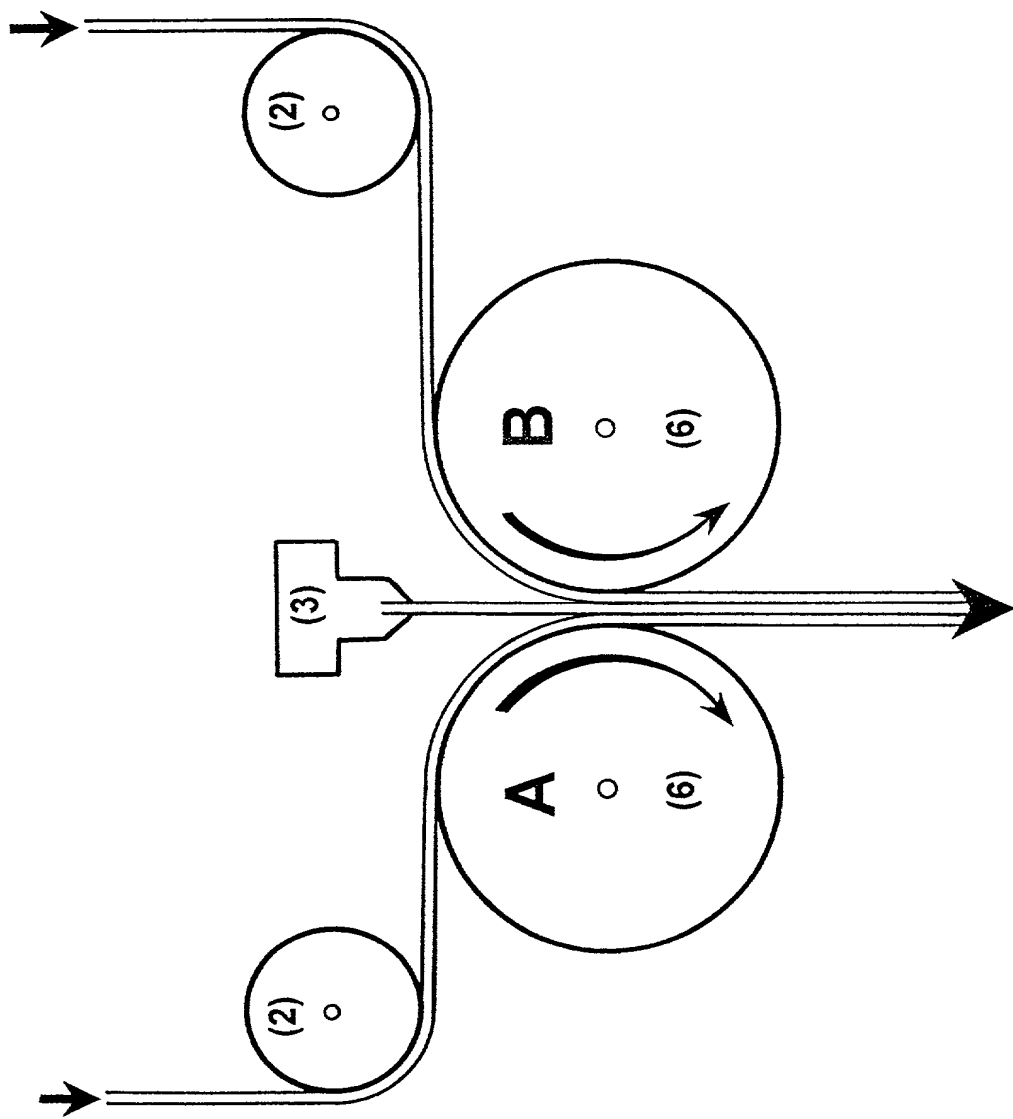
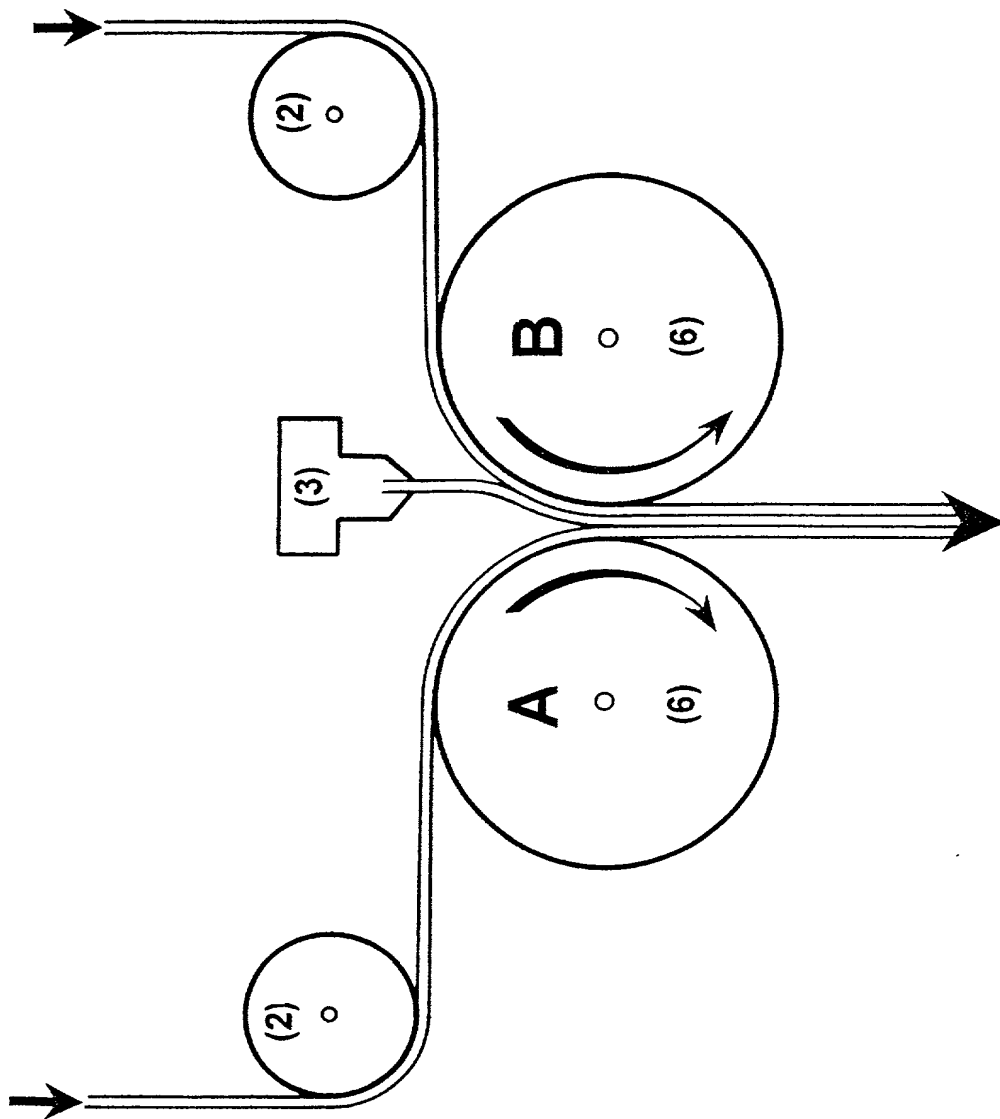


FIG.5A



The diagram shows a mechanical system with two large pulleys, A and B, arranged horizontally. Pulley A is on the left and pulley B is on the right. Both pulleys have a counter-clockwise rotation arrow and are labeled with a center dot and '(6)'. A continuous belt runs from the bottom of pulley A, around its lower half, then up and over the top of pulley B, before descending again. An input shaft enters from the left, passes under pulley A, and connects to a rectangular component labeled '(3)' which has a T-shaped end fitting onto pulley B. This component is also connected to a small circular pulley at the far left labeled '(2)'. An output shaft exits from the right side of pulley B.

FIG.6

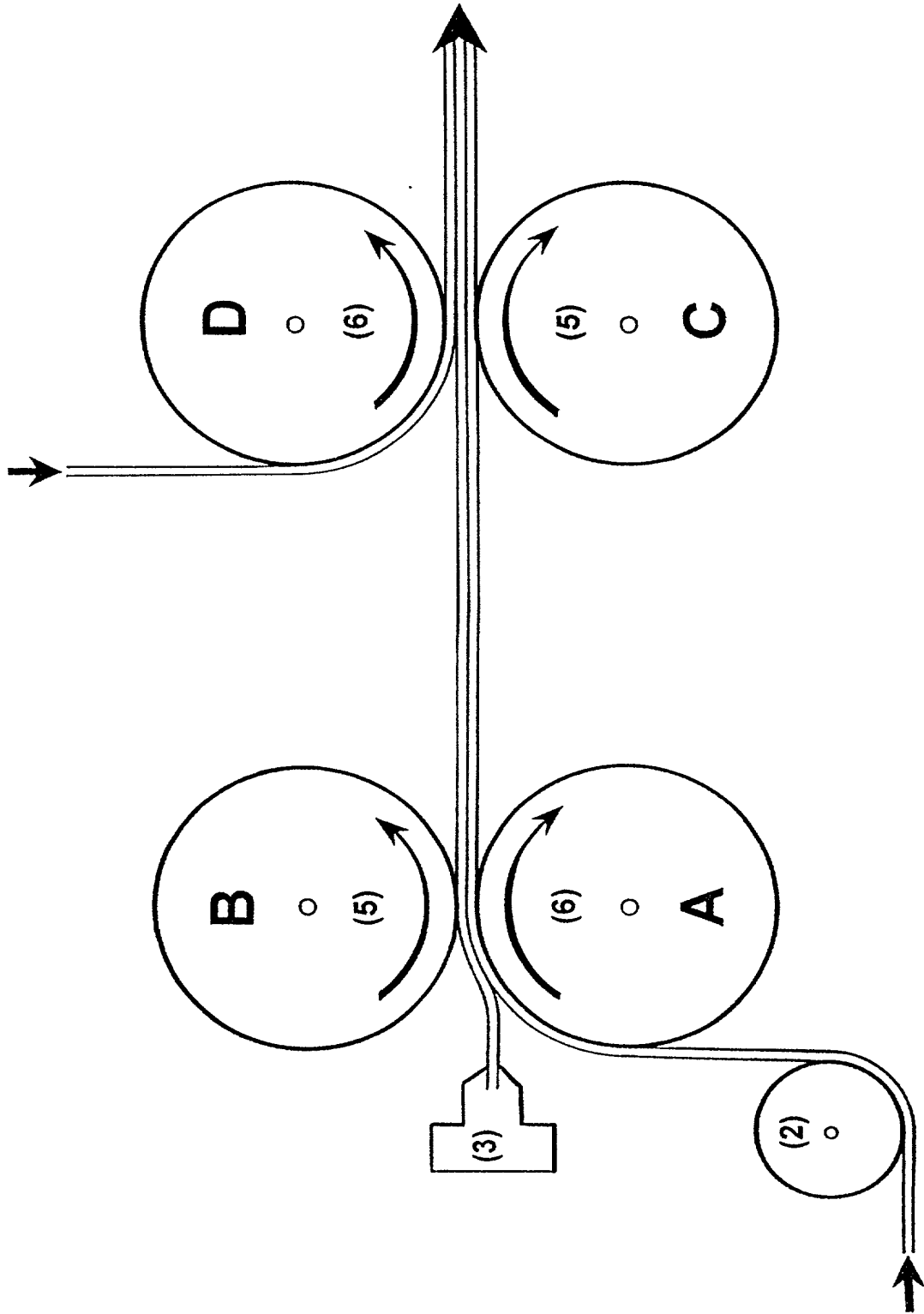
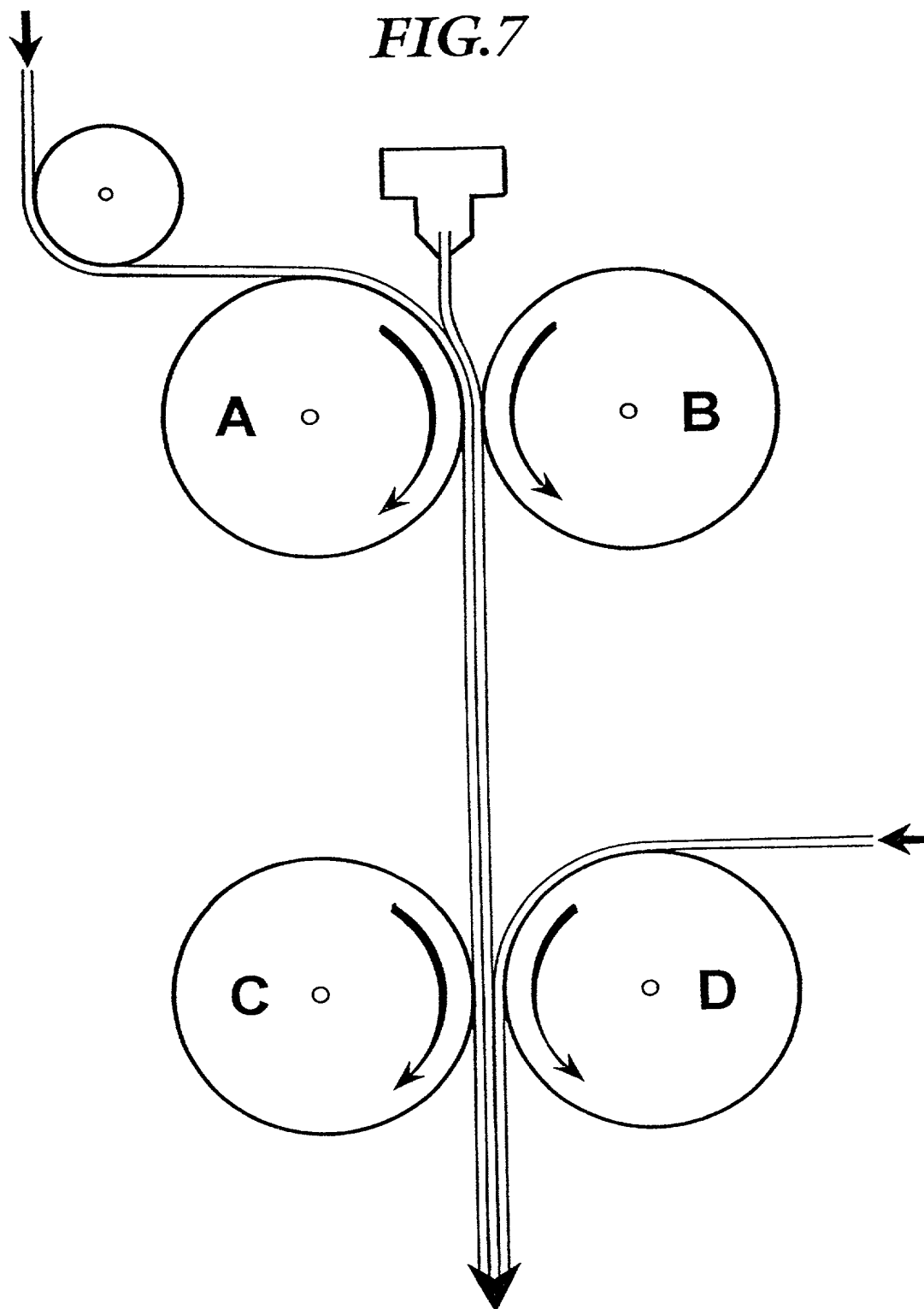


FIG.7



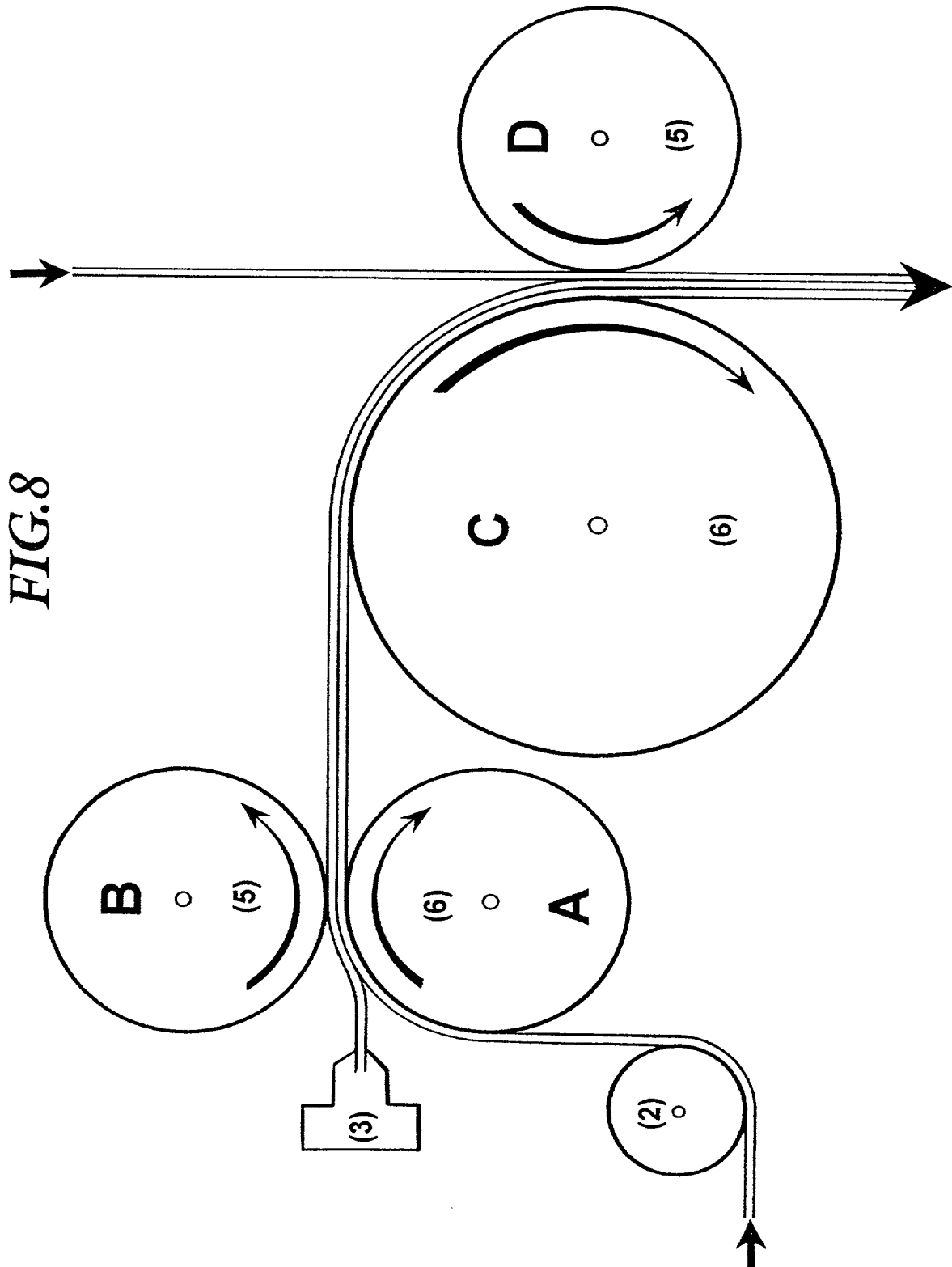


FIG.8

FIG. 9

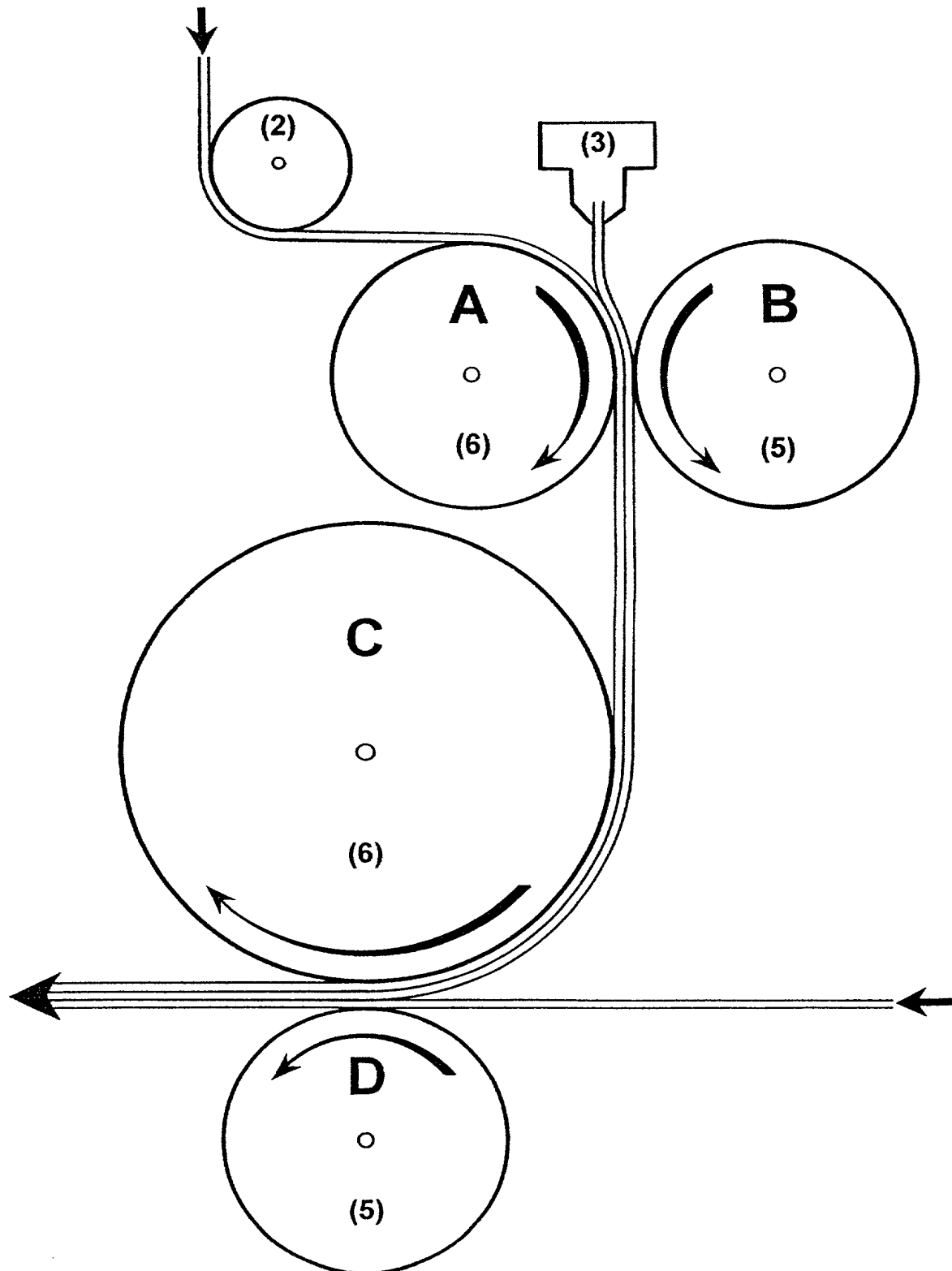


FIG.10

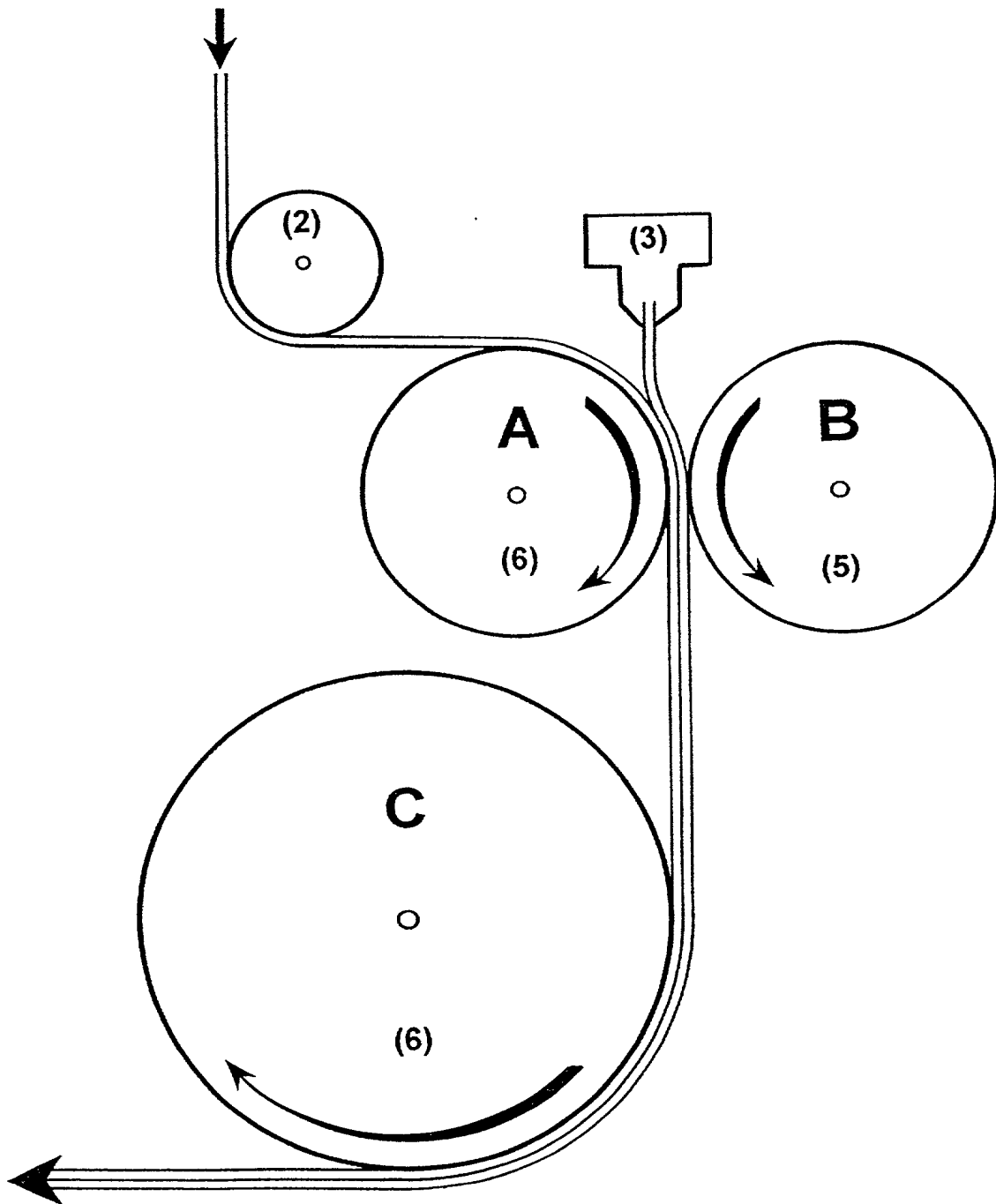


FIG.11

VISCOSITY TEMPERATURE FUNCTION

